#### **6. Optical Resonators**

The microwave resonators are metal boxes or pipes

- (1) to build up large field intensity with moderate input power,
- (2) to act as a special and frequency filter selectively to fields,
- (3) to be used in spectral analyses.

The number of modes with a frequency between v and v + dv per unit volume in a three dimensional resonator is

$$N = \frac{8\pi v^2 n^3}{c^3} dv \tag{1}$$

For a box of  $1 \text{cm}^3$ , a microwave resonator contains at most one mode at a frequency of  $10^9$  Hz. However, at an optical frequency of  $10^{14}$  Hz, the number of modes per unit volume can be as high as  $10^9$  for a bandwidth of  $10^{10}$  Hz, unless the dimension of the resonator is reduced to the size of a wavelength. This problem can be overcome by using open resonators with a pair of mirrors with small areas. Only the mode propagating normal to the mirrors have high Q for meaningful resonance.

In a resonator of distance *l* between mirrors, the beam from one of the mirrors of size  $a_1$  must be smaller than  $a_2$  to avoid losses.



### Fabry-Perot resonator with plane parallel mirrors)

It can be proved, by considering multiple reflections between the mirrors, that, for an incoming electromagnetic radiation of wavelength  $k_0$ , the transmission intensify is given by

$$T = \frac{(1-R_1)(1-R_2)e^{4n_ik_0l}}{(1-\sqrt{R_1R_2}e^{2n_ik_0l})^2 + 4\sqrt{R_1R_2}e^{2n_ik_0l}\sin^2(n_rk_0l)}$$
(2)

where the R's are the reflectance of the mirrors and the index of refraction is a complex number.

For  $n_i = 0$ ,

$$T = \frac{(1 - R_1)(1 - R_2)}{(1 - \sqrt{R_1 R_2})^2 + 4\sqrt{R_1 R_2} \sin^2(kl)}$$
(4)

Case I: 
$$R_I = R_2 = R$$
  
 $T = \frac{(1-R_1)^2}{(1-R)^2 + 4R \sin^2(kl)} = \frac{1}{1 + \frac{4R_1}{(1-R)^2} \sin^2(kl)} = \frac{1}{1 + (\frac{2F}{\pi})^2 \sin^2(\frac{\pi v}{v_F})}$ 
(5)

Where the Finesse is defined by

$$F = \frac{\pi\sqrt{R}}{(1-R)}$$

The linewidth is given by

$$\delta v = \frac{v_F}{F}$$

Meaning?

Case II :  $R_1 = R_2$  and  $n_i \neq 0$ . Case III:  $R_1 \exp(2n_i k_0 l) \approx 1$ 

Finesse and Q-value

Factors affecting linewidth:

- Reflectivity of mirrors
- Length of resonators
- Parallelism of mirrors
- Diffraction losses
- Imperfections in optical materials
- Coherence length

### **Resonator modes:**

Plane-parallel mirrors of finite sizes cannot confine electromagnetic radiation. Stable confinement always involves spherical mirrors.

Hermite Gaussian mode:

From (33) of Lecture 1, the solution for propagating beam in a monogenous medium of index n are:

$$U_{l,m}(x,y) = A_1 \frac{W_0}{W(z)} H_l(\sqrt{2} \frac{x}{W(z)}) H_m(\sqrt{2} \frac{y}{W(z)}) \times e^{\left[-\frac{\rho^2}{W^2(z)} - \frac{jk\rho^2}{2R(z)} - jkz + j(l+m+1)\zeta\right]}$$
(7)

where l,m,n are the order of the modes, the spot size W(z) is

$$W(z) = W_0 [1 + (\frac{z}{z_0})^2]^{1/2}$$
$$z_0 = \frac{\pi W_0^2}{\lambda}$$
The phase factor  $\zeta$  is  
$$\zeta(z) = \tan^{-1}(\frac{z}{z_0}).$$



Stable resonators can be formed by placed two mirrors at  $z_1$  and  $z_2$  with their radii of curvature

matching the curvature of the wavefront.



Starting with a beam with a waist  $W_0$  at z=0, the mirrors placed at  $z=z_1$  and  $z=z_2$  have radii of curvature

$$R_{1} = z_{1} + \frac{z_{0}^{2}}{z_{1}}$$

$$R_{2} = z_{2} + \frac{z_{0}^{2}}{z_{2}}$$
(8)
(9)

A variety of combination of concave and convex mirrors can form a stably resonator.

# **Resonance frequency: p 335**

# Unfolding a resonator

Consider a resonator formed by two mirrors of radii of curvature R1 and R2 separated by a distance R This system can be unfolded into periodic lens sequence



Using the ABCD matrix to represent the position and slop after *m* round trips

$$\begin{bmatrix} y_m \\ \theta_m \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix}^m \begin{bmatrix} y_0 \\ \theta_0 \end{bmatrix}$$
(10)

Consider the relation between consecutive round trips  $y_{m+1} = Ay_m + B\theta_m$  $\theta_{m+1} = Cy_m + D\theta_m$ (11)

By eliminating the angles using the relation,

$$\theta_m = \frac{y_{m+1} - Ay_m}{B}$$
$$\theta_{m+1} = \frac{y_{m+1} - Ay_{m+1}}{B}$$

We have  $y_{m+2} = 2by_{m-1} - F^2 y_m$  (12)

Where 
$$b = \frac{A+D}{2}$$

$$F^{2} = AD - BC = \det|M|$$
(13)

The beam position parameter after m round trips can be related to the initial by  $y_m = y_{max} F^m \sin(m\varphi + \varphi_0)$  (14) where the parameters  $y_{max}$ , and  $\varphi_0$  are to be determined by the initial condition, and  $\varphi = \cos^{-1} \frac{b}{F}$  (15)

For the round trip effect is to reproduce the original position, then F=1 and  $|b| \le 1$  or

$$0 \le (1 + \frac{d}{R_1})(1 + \frac{d}{R_2}) \le 1 \tag{16}$$

It is customary to express the condition for stability as  $0 \le g_1 g_2 \le 1$ 

where  $g_1 = 1 + \frac{d}{R_1}$  $g_2 = 1 + \frac{d}{R_2}$ 

Concave mirrors: R<0.

Discussion of resonator stability diagram.



**Discussions** Planar-planar Planar concave Unstable resonators Diffraction losses due to finite mirror sizes

Homework:

1. Prove Eqs (2) and (4) and write a computer program to plot the transmitted power ( $E^2$ ) as function of distance *l* for a range of variation over a few wavelengths for the case of (4) for various value of R from 0.3 to 1. You may assume that the index of refraction between the mirror is 1.

2. In a symmetric stable resonator,  $R_1 = R_2$ , and  $g_1 = g_2$ . The waist of the beam supported by the resonator is at the center. Express the beam waist using the wavelength, g, and the distance between the mirrors.

3. Find the ratio of the beam sizes at the waist and at mirrors in a symmetric confocal resonator.

4. If two mirrors of radius of curvature of 10 cm and 20 cm, respectively, are used to construct a stable resonator, find the maximum distance between two mirrors.